Debris Flow Hazard Zoning Based on Numerical Simulation in the Wenchuan Earthquake Meizoseismal Areas

Wang Jun^{1, 2, a*}, Yu Yan^{3,b}

¹ Guangzhou Institute of Geography, Guangzhou 510070, China;

²Guangdong Open Laboratory of Geospatial Information Technology and Application; Guangzhou 510070, China;

³ Institute of Mountain Hazards and Environment, Chinese Academy of Sciences, Chengdu 610041, China

^{a*}email: wangjun210@mails.ucas.ac.cn

bemail: yuyan10@mails.ucas.ac.cn

Keywords: Wenchuan earthquake; debris flow; hazard zoning; dynamic process; numerical simulation

Abstract: The Wenchuan earthquake triggered a large number of landslides and collapses in the quake-hit areas, which left a tremendous amount of loose deposits on the slopes and on the valley bottoms. The debris flow pregnant environment has changed dramatically, making the hazard level of debris flow increased greatly. After the earthquake, debris flow hazards occurred frequently and effective hazard assessment of debris flow has become extremely important. The Wu Xianmiao gully in Du Jiangyan city, located in the meizoseismal areas, was selected as the study area. Based on the research of disaster - pregnant environment, a 3-D debris flow numerical simulation platform was established first, then, the hydrological frequency analysis method and the empirical model were used to calculate the debris flow process under the different design frequency (5%, 2% and 1%), the final accumulated scope and depth of debris flow were simulated by the Flow3D software, and the debris flow hazard zonings under the different design frequency were mapped finally.

Introduction

Debris flow is a common natural phenomenon in mountain areas and often brings serious casualties and property loss each year, which seriously affects the economic and social development of mountain areas ^[1]. Especially in the Wenchuan earthquake-stricken areas, the earthquake triggered a large number of loose solid materials resulting in the debris flow pregnant environment and the hazard level of debris flow increased greatly. In the seven years since the earthquake, intense rainfall events have triggered massive debris flows on several occasions (such as the Zhouqu debris flow, the Wenjia gully debris flow and the Hongchun gully debris flow), causing serious casualties and loss of property ^{[2]-[4]}.

As an important means of the disaster non-engineering mitigation, the effective hazard assessment of debris flow has become extremely important. Therefore, this paper focus on the debris flow hazard mapping in the earthquake-hit areas and conduct a case study.

Study area

The Wu Xianmian gully in Du Jiangyan city, located in the meizoseismal areas of Wenchuan earthquake, China, was selected as the study area (Figure 1). The seismic intensity of the study area was XI, which was the maximum seismic intensity of the Wenchuan earthquake. The area extends from 31 05'21" N to 31 05'53" N latitude and 103 35'22" E to 103 36'01" E longitude, covering an area of 1.24 km², with a population of 20 inhabitants. The elevation range of the Wu Xianmian gully is between 965 m and 2140 m, the main channel gradient is 255‰, and the main channel length is approximately 1.8 k m.

Geomorphologically, the study area belongs to the Longmenshan Mountains. The study area has strong tectonic movement and strong erosion, where the main channel is "V"-shaped. The main slope gradient interval of the gully is 30 ° to 40 °, accounting for 68.85% of the entire study area.



Fig. 1 The location of the study area

The disaster-pregnant environment of debris flows

The Wenchuan earthquake triggered a tremendous amount of loose deposits on the slopes and on the valley bottoms. These deposits were remobilized in the form of debris flows in the years following the earthquake. Intensive field investigations indicated that the volume of loose deposits amounted to more than 50×10^4 m³. The abundant loose deposits are shown in Figure 2(a). The channel micro-topography was altered due to erosion and accumulation of loose deposits. The blockage of the gully channel is severe (Figure 2 (b)) and may create a cascade that would be followed by damming, dam breakage and debris flows.



(a) The loose deposits in the gully



(b) The blockage of the main channel

Fig. 2 The loose solid materials and the serious blocking phenomenon in the Wu Xianmiao gully The disaster - pregnant environment of the study area changed dramatically because of the earthquake and the activity frequency of debris flow pre- and post-earthquake also changed sharply. Before the Wenchuan Earthquake, the study area had no debris flows. However, after the earthquake, this area occurred debris flow in 2010 and 2012, affecting the post-earthquake reconstruction and sustainable development.

The 3-D platform of debris flow numerical simulation

There are two ways to access to the 3-D digital terrain, one is use the surveying and mapping instruments directly to obtain 3-D digital terrain, such as GPS, total station, terrestrial 3D laser scanne, the other is by means of aerial photography, obtain the high resolution aerial images and then extract the 3-D digital terrain from aerial images indirectly. In this study, base on geographic information system (GIS), vector the paper topographic map of the Wu Xianmiao gully and obtain elevation points data of the terrain. Write the corresponding program to import the elevation points data into Flow3D

software, the 3-D platform of debris flow numerical simulation can be obtain, which is shown in Figure 3.

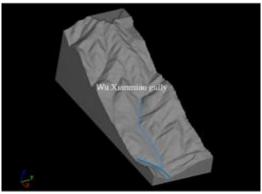


Fig. 3 The 3-D platform of debris flow numerical simulation in Wu Xianmiao gully

The peak discharge and flood hydrograph under the different design frequency

The peak discharge under different design frequency is calculated by the formula proposed by China Institute of Water Resources and Hydropower Research:

$$Q_{p} = 0.278\phi iF = 0.278\phi \frac{s}{\tau^{n}}F$$
 (1)

where, Q_p is the peak discharge (m³/s), ϕ is the peak discharge coefficient: $\phi = f(\mu, \tau^n)$, as μ is the runoff coefficient, F is watershed area (km²), σ is the rain force (mm/h), and σ is the concentration time (h), as:

$$\tau^n = f(m, s, J, L) \tag{2}$$

where, n is the rain index, J is the channel gradient (‰), L is the main channel length (km), and m is the confluence parameter which can be calculated by the formula:

$$m = 0.221\theta^{0.204} \tag{3}$$

where, θ is watershed characteristic parameter, can be expressed as follows:

$$\theta = \frac{L}{J^{1/3} F^{1/4}} \tag{4}$$

Above parameters is obtained by handbook of the storm flood calculation in Sichuan province (1984), and the key parameters are listed in Table 1.

	<u> </u>					
	Watershed	Channel	Channel	Watershed	Confluence	Runoff
Watershed	area	length	gradient	characteristic	parameter	coefficient
	/F/km ²	/L/km	/J/‰	parameter / θ	/m	$/\mu$
Wu	1.24	1 0	0.255	2.600	0.270	2.456
Xianmiao	1.24	1.8	0.255	2.690	0.270	3.456

Table 1 The parameters of the watershed characteristic parameters in the study area According to the handbook of the storm flood calculation in Sichuan province (1984), the peak discharge under the different design frequency (5%, 2% and 1%) can be obtained. After this, the typical flood amplification method is used to calculate the design flood hydrograph.

Calculation of debris flow discharge hydrograph under the different design frequency

The debris flow runoff process is controlled by the water flow runoff and the amounts of started loose materials, which can be obtained by combining water flow process and appropriate debris flow parameters. Based on a large number of experiments and field observations, Chinese debris flow scholars proposed the empirical formula calculating debris flow discharge, which is widely used in China [17]:

$$Q_C = (1 + \phi) \mathcal{Q}_P \mathcal{Q}_C \tag{5}$$

in which Q_c is the debris flow peak discharge; Q_p is the water flow peak discharge; D_c is the channel blockage parameter, its empirical value is shown in Table 4; φ is the sediment correction coefficient, can be calculated by the formula:

$$\phi = (\gamma_C - \gamma_W) / (\gamma_H - \gamma_C) \tag{6}$$

in which γ_c and γ_w are the unit weight of debris flow and water, respectively; γ_H is the weight of solid materials in debris flow, always is 27 kN/m³.

The degree of blockage	No blockage	Slight blockage	Moderate blockage	Severe blockage
D_{C}	1	1.5	2	2.5

Table 2 The channel blockage parameter [17]

To this end, the debris flow runoff process can be obtained combining the water flow confluence process and the empirical formula. Finally, the calculated parameters are shown in Table 3 and debris flow processes under the different design frequency (5%, 2% and 1%) are shown in Figure 4.

Design frequency	Blockage parameter/ D_c	The density of debris flow/ ρ _c /g/cm ³	The density of loose materials/ ρ_H /g/cm ³	Sediment correction coefficient/\$\phi\$	Water flow peak discharge /Qp/m ³ /s	Debris flow peak discharge Qc/m ³ /s
5%	2.5	1.717	2.70	0.737	36.26	157.35
2%	2.5	1.717	2.70	0.737	42.936	186.33
1%	2.5	1.717	2.70	0.737	47.86	207.70

Table 3 The peak discharge of debris flow under the different design frequency in the study area

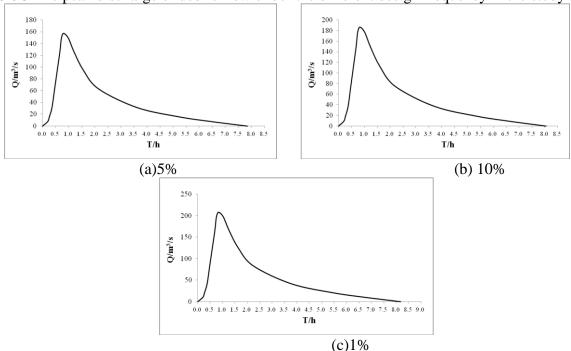


Fig. 4 The discharge hydrograph of debris flow under the different design frequency in the Wu Xianmiao gully

Numerical simulation and hazard zonings of debris flow

In Flow3D, use the debris flow discharge hydrograph as the initial condition and use the 3-D platform of debris flow numerical simulation as boundary condition to conduct debris flow numerical simulation. The debris flow parameters used in numerical simulation is shown in Table 4.

Debris flow property	Density /g/cm ³	Yield stress /Pa	Coefficient of viscosity	Bed roughness
Bingham	1.717	20	0.5	0.1

Table 4 The debris flow parameters used in numerical simulation

Through debris flow numerical simulation, the scope and depth of debris flow deposits can be obtained.

Use the debris flow depth as the parameter to conduct debris flow hazard zonings, the hazard classified criteria in the study area is show in Table 5.

Debris flow hazad class	Depth/m
Low hazard degree	h≤1m
Moderate hazard degree	1m <h td="" ≤3m<=""></h>
High hazard degree	3m <h td="" ≤6<=""></h>
Extremely high hazard degree	h>6m

Table 5 The debris flow hazard classified criteria in the study area

Base on the debris flow simulation and the hazard classified criteria, the debris flow hazard zonings under the different design frequency in the study area is shown in Figure 5.

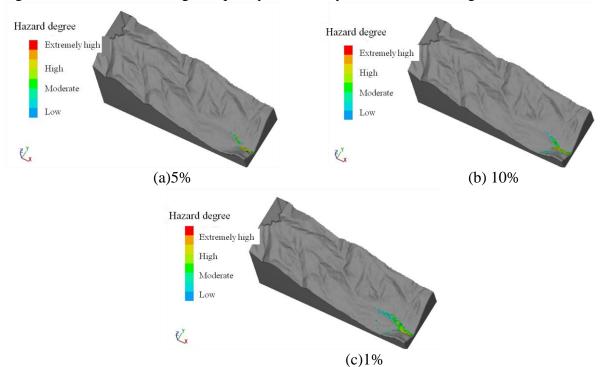


Fig. 5 The debris flow hazard zonings under the different design frequency in the study area

Acknowledgements

Financial support was provided by talent fund of Guangzhou Institute of Geography (NO. 2015157ZGD), National Natural Science Foundation (NO. 41372331), the international cooperation project of the Ministry of Science and Technology (NO. 2013DFA21720), and Guangdong province water conservancy science and technology innovation project (NO. 2011-19).

References

- [1] J. Wang, Y. Yu, S. Yang, G. H. Lu, G. Q. Ou, A modified certainty coefficient method (M-CF) for debris flow susceptibility assessment: A case study for the Wenchuan earthquake meizoseismal areas, Journal of Mountain Science. 11(5) (2014) 1286-1297.
- [2] B. Yu, Y. Ma and F. Y. Wu, Investigation of severe debris flow hazards in Wenjia gully of Sichuan province after the Wenchuan earthquake, Journal of Engineering Geology 18(6) (2010) 827-836.
- [3] Y. You, J. F. Liu and X. Z. Chen, Debris flow and its characteristics of Subao river in Beichuan county after 5.12 Wenchuan earthquake, Journal of Mountain Science, 28(3)(2010) 358-366.
- [4] J. Wang, Y. Yu, H. L. Pan, C. Qiao, G. Q. Ou, Debris flow formation process and critical hydrodynamic conditions in the meizoseismal areas of Wenchuan earthquake. Journal of Mountain Science 12(3) (2005) 699-710.